

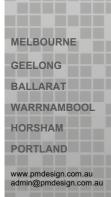
#### 20/04/2023

Our ref: 15718 Doc rev: Α

### **Stormwater Management System** Report

### 122/124 Lonsdale Street, Hamilton









#### **Document Revision Summary**

Revision	Date	Section	Description	Authorized		
А	20/04/2023		Issued for Approval.	DC		



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#### 2 INTRODUCTION

This report has been prepared by PM Design Group for the construction of a new medical facility namely the South West Hospital, at 122/124 Lonsdale St, Hamilton. An aerial view of the locality is shown as Figure 1.



Figure 1: Aerial View



#### 3 THE DEVELOPMENT

The site is approximately 1 857m², comprising the consolidation of 122 and 124 Lonsdale Street. These existing sites comprise two existing structures and an existing asphalt playing court area together with paved walkways. The remainder the site areas has an established grassed covering.

It is proposed to demolish the existing structures and undertake the construction of 1 new single storey building and a new parking area, along with minimal paving of the site for walkways on the Eastern and Western building envelopes. *Appendix A* contains the proposed overall post development site plan.

In accordance with the IDM it is proposed to limit site discharge to the predevelopment flow for a 10% AEP storm.

To facilitate this outcome a combination of two new 5 000lt above ground rainwater water storage tanks and on surface detention at the proposed new carpark will be used to catch roof and paved area water flows for the sub-catchments, this captured water will then be discharged at a reduced flow rate via. orifice pipes and plates in each system thereby limiting the overall post development flow to the overall site predevelopment flow. Overflow will be provided via DN100 PVC to the LPOD.

Water Sensitive Urban Design best practice procedures will also be adopted to minimise pollutant impact to receiving waterways.

Overall site pavement levels and grading will be determined by PM Design Group. For the purposes of restricted flow calculations, all pavement and landscaped areas are considered as either infiltrating or discharging unrestrained to the surrounding Road Reserves



#### 2 INTRODUCTION

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Figure 1: Aerial View



#### 5 POST DEVELOPMENT FLOWS

Post development restrained flow catchments have been calculated as per the site plan attached as *Appendices A and B*. These catchments are summarised below:

**Table 2: Post-Development Restrained Catchment Summary** 

Location	Area (A) ha	Co-efficient (C <sub>w</sub> )	Effective Area (AC <sub>w</sub> )
Roof West	0.017900	0.95	0.01701
Roof East	0.034400	0.95	0.03268
Parking areas	0.051000	0.95	0.04845
Total	0.103300	∑ Ae (ha)	0.098135

It is proposed that the post-development driveways and front landscaped areas discharge unrestrained. The resultant flow has been calculated below, using 1in5 ARI, Time of Concentration of 10 minutes and the Rational Method:

**Table 3: Post-Development Un-Restrained Catchment Summary** 

Location	Area (A) ha	Co- efficient (C <sub>w</sub> )	Effective Area (AC <sub>w</sub> )	∑(AC <sub>w</sub> ) ha	l mm/hr	Q m³/s
Landscape	0.0660	0.25	0.016500			
Paving	0.0164	0.95	0.015580			
Total	0.0824			0.03208	90.8	0.008091

Removing this flow from the adopted pre-development discharge gives a resultant discharge limit for the restrained catchments as follows:

Pre-development flow - Unrestrained Post Development Flow = Q restrict  $0.011709 - 0.008091 = \underline{0.003618 \text{ m}^3/\text{s}}$ 

Therefore, allowable discharge from the catchment post-development will be limited to 3.618 l/s, for the 10% AEP design storm. These have been distributed proportionally within the different internal catchment zones and each has been restrained via. the use of either orifice pipes or orifice plates. These overall restrictions will limit post development flows to the predevelopment flow for the site. The overall system will allow for the surcharge flows to be directed to the Lonsdale Street Road Reserve in a safe manner. Refer to the calculations in Appendix D of this report for the relevant storage requirements and control measures.



#### 3 THE DEVELOPMENT

The site is approximately 1 857m², comprising the consolidation of 122 and 124 Lonsdale Street. These existing sites comprise two existing structures and an existing asphalt playing court area together with paved walkways. The remainder the site areas has an established grassed covering.

It is proposed to demolish the existing structures and undertake the construction of 1 new single storey building and a new parking area, along with minimal paving of the site for walkways on the Eastern and Western building envelopes. *Appendix A* contains the proposed overall post development site plan.

In accordance with the IDM it is proposed to limit site discharge to the predevelopment flow for a 10% AEP storm.

To facilitate this outcome a combination of two new 5 000lt above ground rainwater water storage tanks and on surface detention at the proposed new carpark will be used to catch roof and paved area water flows for the sub-catchments, this captured water will then be discharged at a reduced flow rate via. orifice pipes and plates in each system thereby limiting the overall post development flow to the overall site predevelopment flow. Overflow will be provided via DN100 PVC to the LPOD.

Water Sensitive Urban Design best practice procedures will also be adopted to minimise pollutant impact to receiving waterways.

Overall site pavement levels and grading will be determined by PM Design Group. For the purposes of restricted flow calculations, all pavement and landscaped areas are considered as either infiltrating or discharging unrestrained to the surrounding Road Reserves



#### 7 MAJOR STORM MANAGEMENT

The finished site grading is being determined by others and shall be set such that the major storm flows are directed to a grated pits around the site, then piped to the front of the property where it may surcharge and flow overland to the nominated Legal Point of Discharge. The existing topography of the site facilitates the draining to the Lonsdale Steet Road reserve. The site shall be graded such that these natural surface flows are maintained.

#### 8 WATER SENSITIVE URBAN DESIGN

WSUD criteria will be met by the following methodology:

- Additional treatment for the paved walkways, parking and roof areas will be via. the adoption of rainwater tanks and onsite carpark detention.
- Use of pit(s) with silt sumps, sized as below.

In accordance with the requirements of the planning permit we have used the results of the STORM tool calculations with a resultant STORM rating of 121%. The output from the STORM tool which is included in *Appendix E*.

Pit Sump Sizing:

2/No. 600 x 600mm Grated Sump Pits will be installed to collect silt from the surface water flows. These pits will have a minimum 300 mm deep sump for silt collection, sized as follows:

- Roof water is considered fully treated and is included in the calculation.
- Post Development Un-Treated Surface Area totals 0.1172 ha
- Sediment Accumulation Rate of 1.6m³/ha/annum (WSUD Engineering Procedures, CSIRO 2006)
- Annual Accumulation = 0.1172 x 1.6 = 0.1875 m³
- Target Cleaning Frequency = Once a Year
- Pit Sump Dimensions: 0.60m W x 0.60m L x 0.3m D; Volume = 0.108m³ x 2/No. = 0.216m³

Sump Capacity = Cleaning Frequency Accumulation

0.216/0.1875 = Every 1.152 Years



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Figure 1: Aerial View



Alternatively, onsite tank gauges can help those familiar with the tank know if the tank is not working correctly.

#### <u>Pumps</u>

Maintenance should occur as per the chosen Manufacturer's specifications. All strainers and filters should be cleaned every 6 months. Good quality pump should provide trouble free service for up to 10 years.

#### Commissioning

#### Rainwater Tank

All rainwater tanks should be washed or flushed out prior to use. All inlets and outlets should be correctly sealed to prevent insects entering. Connection to all toilets and laundry in the development should be tested (dye test or equivalent).

Please note if new roof coating or paint is to be installed then the first few run-offs after installation need to be discarded.

#### **Pumps**

Commissioning should occur as per the chosen Manufacturer specifications.

#### Summarv

The following needs to occur onsite to ensure compliance with WSUD requirements and maintain operation of rainwater tank and connections onsite.

Task	When?	Requirement
Inspect Rainwater tanks	Every 6 months	Check for any damage/compression     Mosquitoes infestation
	Every 2 years	Sludge Build up — if sludge build up occurs a vacuum tank needs to be called out to site.
Inspect roofs & gutters	Every 6 months	Clean out of leaves / debris.     Remove any overhanging branches onsite.



#### 10 CONCLUSION

This Stormwater Management Plan outlines the methods by which the site may be drained, in support of the planning application.

- Design Storm nominated as 10% AEP.
- Minor storm managed using storage and a dual chamber orifice pit.
- · Major storm discharge to LPOD without affecting other properties.
- WSUD criteria has been considered.

Report Prepared By:

Asheen Singh Civil Engineer

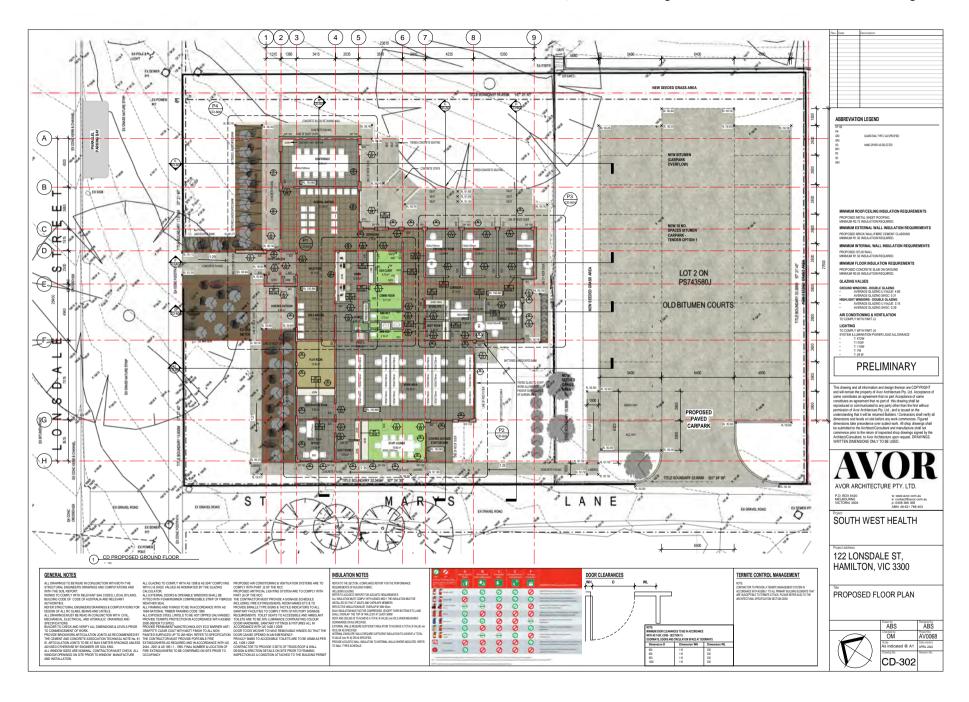
Email: asheen.singh@pmdesign.com.au

Approved By:

Darren Cuttler Civil Team Leader

Email: darren.cuttler@pmdesign.com.au











## DESIGN GROUP Engineering Solutions

Project: 15718
Date: 24/03/2023
Engineer: A.Singh

#### Intensity, Frequency and Duration (IFD) Table

122/124 Lonsdale Street,

Location: HAMILTON
Date: 24/03/2023
Units: mm/hr

Duration		Annual Exceedence Probability (AEP)							
(mins)	63.20%	50%	20%	10%	5%	2%	1%		
1	79.7	90.3	127.0	154.0	184.0	226.0	262.0		
2	68.8	77.7	108.0	130.0	154.0	188.0	215.0		
3	61.1	69.1	96.2	116.0	138.0	168.0	194.0		
4	55.3	62.6	87.4	106.0	126.0	154.0	178.0		
5	50.7	57.4	80.4	97.7	116.0	143.0	165.0		
6	47.0	53.2	74.6	90.8	108.0	133.0	154.0		
10	36.9	41.9	58.9	71.8	85.6	106.0	123.0		
15	29.8	33.8	47.5	57.9	69.0	85.3	99.0		
20	25.3	28.7	40.3	49.1	58.4	72.2	83.8		
25	22.1	25.1	35.2	42.9	51.0	63.0	73.0		
30	19.8	22.4	31.4	38.2	45.5	56.1	65.0		
45	15.3	17.3	24.2	29.4	35.0	43.0	49.8		
60	12.7	14.3	20.0	24.3	28.8	35.4	40.9		
90	9.7	10.9	15.2	18.5	21.9	26.9	31.0		
120	8.0	9.0	12.5	15.2	18.0	22.1	25.5		
180	6.0	6.8	9.5	11.5	13.7	16.8	19.4		
270	4.6	5.1	7.2	8.7	10.4	12.8	14.8		
360	3.7	4.2	5.9	7.2	8.5	10.5	12.2		
540	2.8	3.2	4.5	5.4	6.5	8.0	9.3		
720	2.3	2.6	3.7	4.5	5.3	6.6	7.7		
1080	1.7	2.0	2.8	3.4	4.0	5.0	5.8		
1440	1.4	1.6	2.3	2.7	3.3	4.1	4.7		
1800	1.2	1.4	1.9	2.3	2.8	3.4	4.0		
2160	1.1	1.2	1.7	2.0	2.4	3.0	3.5		
2880	0.9	1.0	1.3	1.6	1.9	2.4	2.8		
4320	0.6	0.7	1.0	1.2	1.4	1.7	1.9		
5760	0.5	0.6	0.8	0.9	1.1	1.3	1.5		
7200	0.4	0.5	0.6	0.8	0.9	1.0	1.2		
8640	0.4	0.4	0.6	0.6	0.7	0.9	1.0		
10080	0.3	0.4	0.5	0.6	0.6	0.8	0.9		

http://www.bom.gov.au/water/design Rainfalls/revised-

Source: ifd/

Site Address: 122/124 Lonsdale St , HAMILTON
Single Point Map Co-Ordinates: -37.739658, 142.026701

Accessed: 24/03/2023





# DESIGN GROUP Engineering Solutions

 Project:
 15718

 Date:
 24/03/2023

 Engineer:
 A.Singh

#### Intensity, Frequency and Duration (IFD) Table

122/124 Lonsdale Street,

Location: HAMILTON
Date: 24/03/2023
Units: mm/hr

Duration	Annual Exceedence Probability (AEP)							
(mins)	63.20%	50%	20%	10%	5%	2%	1%	
1	79.7	90.3	127.0	154.0	184.0	226.0	262.0	
2	68.8	77.7	108.0	130.0	154.0	188.0	215.0	
3	61.1	69.1	96.2	116.0	138.0	168.0	194.0	
4	55.3	62.6	87.4	106.0	126.0	154.0	178.0	
5	50.7	57.4	80.4	97.7	116.0	143.0	165.0	
6	47.0	53.2	74.6	90.8	108.0	133.0	154.0	
10	36.9	41.9	58.9	71.8	85.6	106.0	123.0	
15	29.8	33.8	47.5	57.9	69.0	85.3	99.0	
20	25.3	28.7	40.3	49.1	58.4	72.2	83.8	
25	22.1	25.1	35.2	42.9	51.0	63.0	73.0	
30	19.8	22.4	31.4	38.2	45.5	56.1	65.0	
45	15.3	17.3	24.2	29.4	35.0	43.0	49.8	
60	12.7	14.3	20.0	24.3	28.8	35.4	40.9	
90	9.7	10.9	15.2	18.5	21.9	26.9	31.0	
120	8.0	9.0	12.5	15.2	18.0	22.1	25.5	
180	6.0	6.8	9.5	11.5	13.7	16.8	19.4	
270	4.6	5.1	7.2	8.7	10.4	12.8	14.8	
360	3.7	4.2	5.9	7.2	8.5	10.5	12.2	
540	2.8	3.2	4.5	5.4	6.5	8.0	9.3	
720	2.3	2.6	3.7	4.5	5.3	6.6	7.7	
1080	1.7	2.0	2.8	3.4	4.0	5.0	5.8	
1440	1.4	1.6	2.3	2.7	3.3	4.1	4.7	
1800	1.2	1.4	1.9	2.3	2.8	3.4	4.0	
2160	1.1	1.2	1.7	2.0	2.4	3.0	3.5	
2880	0.9	1.0	1.3	1.6	1.9	2.4	2.8	
4320	0.6	0.7	1.0	1.2	1.4	1.7	1.9	
5760	0.5	0.6	0.8	0.9	1.1	1.3	1.5	
7200	0.4	0.5	0.6	0.8	0.9	1.0	1.2	
8640	0.4	0.4	0.6	0.6	0.7	0.9	1.0	
10080	0.3	0.4	0.5	0.6	0.6	0.8	0.9	

http://www.bom.gov.au/water/design Rainfalls/revised-

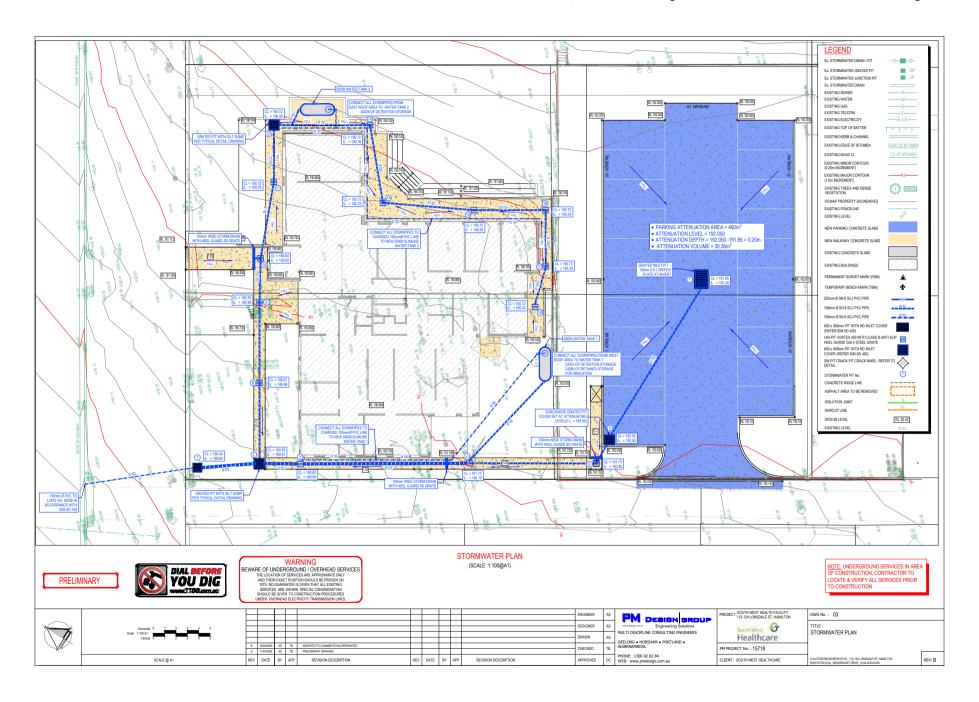
Source: ifd/ Accessed: 24/03/2023

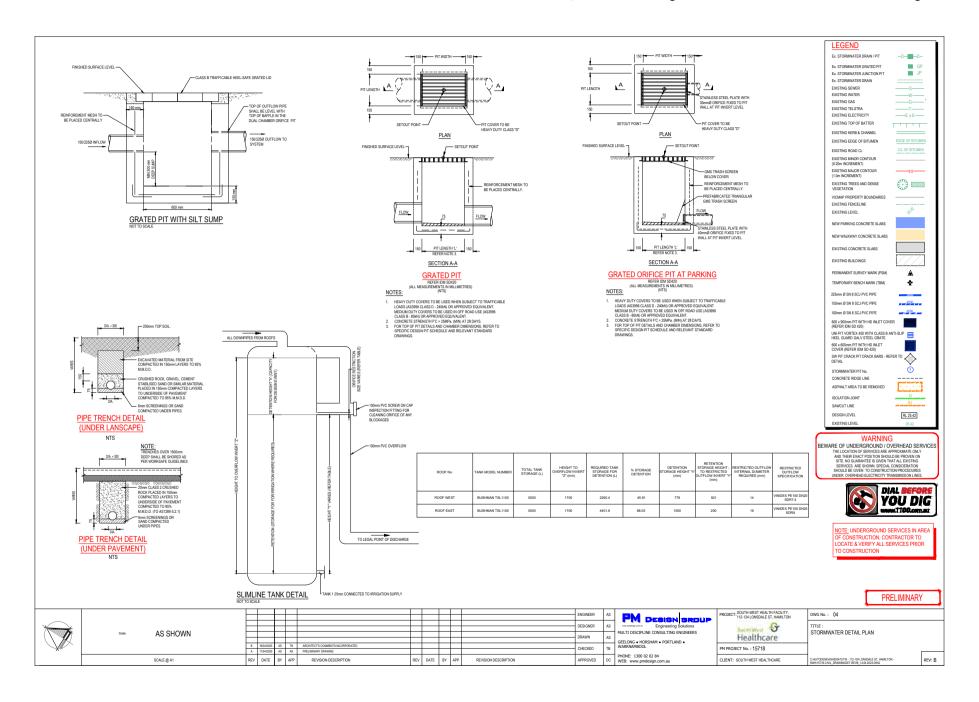
Site Address: 122/124 Lonsdale St , HAMILTON
Single Point Map Co-Ordinates: -37.739658, 142.026701















 Project No.
 15718

 Date:
 19/04/2023

 Eng:
 A.Singh

To be input by user

Area:

Carpark

Item	A (ha)	С	Ae (ha)
Carpark	0.0510	0.9500	0.0485
Total	0.0510		0.0485

Design Storm:

Effective Catchment Area (Ae) = Restricted outflow requirement 10% AEP 0.0485 ha 0.001786 m³/s

Storage requirement is highest value of S  $_{max}$  calculated in the table below Critical storm duration is the storm duration when S  $_{max}$  occurs

Continue table until a clear Smax is calculated

Storm Duration	10% AEP	Constant Input	Rainfall Input	l <sub>p</sub>	$Q_p$	<b>V</b> <sub>1</sub>	S <sub>max</sub>
(min)	Intensity (mm/hr)	(m³/s)	(m³/s)	(m³/s)	(m³/s)	(m³)	(m <sup>3</sup> )
5	97.7	0.00	0.0131	0.0131	0.0018	3.94	3.409
6	90.8	0.00	0.0122	0.0122	0.0018	4.40	3.756
10	71.8	0.00	0.0097	0.0097	0.0018	5.80	4.726
15	57.9	0.00	0.0078	0.0078	0.0018	7.01	5.405
20	49.1	0.00	0.0066	0.0066	0.0018	7.93	5.786
25	42.9	0.00	0.0058	0.0058	0.0018	8.66	5.981
30	38.2	0.00	0.0051	0.0051	0.0018	9.25	6.039
45	29.4	0.00	0.0040	0.0040	0.0018	10.68	5.860
60	24.3	0.00	0.0033	0.0033	0.0018	11.77	5.343
90	18.5	0.00	0.0025	0.0025	0.0018	13.44	3.799
120	15.2	0.00	0.0020	0.0020	0.0018	14.73	1.867
180	11.5	0.00	0.0015	0.0015	0.0018	16.72	-2.577

Storage Volume Required (m³)

Critical Storm Duration (min)

Storage Volume from Car Park = 1/3 x B x H

Total Volume available =

	6.04
	30.00
m³	30.36
m³	30.36

Where B = Area(460m² of parking attenuation

Where H = 0.20m (height of attenuation at surface)

> 6.039 m<sup>3</sup>

NOTES:

 $Q=C_{\!d}A\sqrt{2gh}$ 

Orifice Area= Q/CdV2gh
Orifice Area= 0.0009 m²
Orifice Diameter= 0.034 m

34 therefore use 40mm dia.

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	Project:	G.15718
	Date:	19/04/2023
	Engineer:	A.Singh

**Storage Sizing - Roof East** 

Site:

122/124 Lonsdale St , HAMILTON

Design Storm: Catchment Area (A) = Restricted outflow requirement

**10% AEP** 0.0344 ha 0.00120488 m<sup>3</sup>/s

Storage requirement is highest value of S  $_{\it max}$  calculated in the table below Critical storm duration is the storm duration when S  $_{\it max}$  occurs

Continue table until a clear S  $_{\it max}$  is calculated

Storm Duration	10% AEP	Rainfall Input	I <sub>p</sub>	$\mathbf{Q}_{p}$	$V_1$	$\mathbf{S}_{max}$
(min)	Intensity (mm/hr)	(m³/s)	(m³/s)	(m³/s)	(m³)	(m³)
5	97.7	0.00934	0.00934	0.001205	2.80073	2.43927
6	90.8	0.00868	0.00868	0.001205	3.12352	2.68976
10	71.8	0.00686	0.00686	0.001205	4.11653	3.39361
15	57.9	0.00553	0.00553	0.001205	4.97940	3.89501
20	49.1	0.00469	0.00469	0.001205	5.63013	4.18428
25	42.9	0.00410	0.00410	0.001205	6.14900	4.34169
30	38.2	0.00365	0.00365	0.001205	6.57040	4.40162
45	29.4	0.00281	0.00281	0.001205	7.58520	4.33204
60	24.3	0.00232	0.00232	0.001205	8.35920	4.02165
90	18.5	0.00177	0.00177	0.001205	9.54600	3.03967
120	15.2	0.00145	0.00145	0.001205	10.45760	1.78250
180	11.5	0.00110	0.00110	0.001205	11.86800	-1.14465

$O = C \cdot A \sqrt{2ab}$	Storage Required	(m³)	4.40162
$Q=C_dA\sqrt{2gh}$	Critical Storm Duration	(min)	30

Storage			
Height (Z)	1.7 m	Invert of Overflow to Pump Outlet	
Capacity	5000 L	Nominal, from supplier	Adopt Bushman TSL1100
Area	2.941176 m <sup>2</sup>	Cross sectional area of tank (Capacity	divided by Height)
Detention Volume	4401.62 L	(from Storage Required)	
Supply Volume	598.38 L	Capacity, less Storage Required - used for Treatment	
Supply Depth (Y)	0.2 m	Height, less "Head" (Below)	
Head (h)	1.5 m	Detention Volume divided by Area	
Pipe Co-Efficient	0.8		
Area	0.00028 m <sup>2</sup>	- Restricted Outflow Calculation	on
Internal Diameter	19 mm		
	A	dopt VINIDEX PE100 DN25 SDR9	



Project:	G.15718
Date:	19/04/2023
Engineer:	A.Singh

**Storage Sizing - Roof West** 

Site:

122/124 Lonsdale St , HAMILTON

Design Storm: Catchment Area (A) = Restricted outflow requirement 10% AEP 0.0179 ha 0.00062696 m³/s

Storage requirement is highest value of S  $_{max}$  calculated in the table below Critical storm duration is the storm duration when S  $_{max}$  occurs

Continue table until a clear S  $_{max}$  is calculated

Storm Duration	10% AEP	Rainfall Input	I <sub>p</sub>	$\mathbf{Q}_{p}$	$V_1$	$S_{max}$
(min)	Intensity (mm/hr)	(m³/s)	(m³/s)	(m³/s)	(m³)	(m³)
5	97.7	0.00486	0.00486	0.000627	1.45736	1.26927
6	90.8	0.00451	0.00451	0.000627	1.62532	1.39962
10	71.8	0.00357	0.00357	0.000627	2.14203	1.76586
15	57.9	0.00288	0.00288	0.000627	2.59103	2.02677
20	49.1	0.00244	0.00244	0.000627	2.92963	2.17729
25	42.9	0.00213	0.00213	0.000627	3.19963	2.25919
30	38.2	0.00190	0.00190	0.000627	3.41890	2.29038
45	29.4	0.00146	0.00146	0.000627	3.94695	2.25417
60	24.3	0.00121	0.00121	0.000627	4.34970	2.09266
90	18.5	0.00092	0.00092	0.000627	4.96725	1.58169
120	15.2	0.00076	0.00076	0.000627	5.44160	0.92752
180	11.5	0.00057	0.00057	0.000627	6.17550	-0.59562

$-C_1A \sqrt{2ab}$	Storage Required	(m³)
$O=C_dA\sqrt{2g\hbar}$	<b>Critical Storm Duration</b>	(min)

Storage

Q

Height (Z)	1.8 m	Invert of Overflow to Pump Outlet		
Capacity	3000 L	Nominal, from supplier	Adopt Bushman TSL660	
Area	1.666667 m <sup>2</sup>	Cross sectional area of tank (Capacity	divided by Height)	
Detention Volume	2290.38 L	(from Storage Required)		
Supply Volume	709.62 L	Capacity, less Storage Required - used for Treatment		
Supply Depth (Y)	0.43 m	Height, less "Head" (Below)		
Head (h)	1.37 m	Detention Volume divided by Area		
Pipe Co-Efficient	0.8			
Area	0.00015 m <sup>2</sup>	- Restricted Outflow Calculation	on	
Internal Diameter	14 mm			
	Ad	opt VINIDEX PE100 DN20 SDR7.4		

2.29038

30



#### 15 APPENDIX E

Storm Tool Calculator



## Melbourne STORM Rating Report

TransactionID: 1565039

Municipality: SOUTHERN GRAMPIANS

Rainfall Station: HAMILTON

Address: 122/124 Lonsdale Street

SWH Hamilton VIC

Assessor: Asheen Singh
Development Type: Commercial/Retail

Allotment Site (m2): 1.857.00 STORM Rating %: 121

Description	Impervious Area (m2)	Treatment Type	Treatment Area/Volume (m2 or L)	Occupants / Number Of Bedrooms	Treatment %	Tank Water Supply Reliability (%)
Roofs	523.00	Rainwater Tank	10,000.00	25	150.20	79.00
Carpark	510.00	None	510.00	0	0.00	0.00
Landscaping	660.00	Infiltration Sand	660.00	Q	222.00	0.00
Walkways	164.00	None	0.00	0	0.00	0.00

Date Generated: 20-Apr-2023 Program Version: 1.0.0

Tender 076-23 Supply of Road Making Materials			
QUARRY	MATERIAL	AVAILABILITY (Notice period required for pick up)	
Rigby Bros Pty Ltd	20mm Crushed Rock (Class 2 & 3) 40mm Crushed Rock (Class 3 & 4) 5mm Dust (Blue) 100 / 200mm Metal (Blue) 100 / 200mm Metal (Brown) Sand (fine) Sand (course)	5 to 10 days	
LK Earthmovers Pty Ltd	Shot Rock  20mm Crushed Rock (class 3) 19mm Crusher Run 40mm Crusher Run		
Mooree Partnership	50mm Ballast 20mm Crushed Rock (Class 3 & 4) 20mm Crushed Rock (NDCR) 40mm Crushed Rock (NDCR) 40mm Crushed Rock (Class 3 & 4) 20 / 40mm Drainage 40 / 60mm Drainage Gravel loose at pit 100 / 200mm Metal (Blue) 100 / 200mm Metal (Brown) Shot Rock Spalls	2 weeks 1 month 2 weeks 2 weeks 2 weeks 2 weeks 2 weeks 2 weeks	
Walkers Earthworks Pty Ltd	20mm Crushed Rock (Class 2, 3 & 4) 20mm Crushed Rock (NDCR) 40mm Crushed Rock (Class 3) 40mm Crushed Rock (NDCR) 20 / 40mm Drainage Gravel loose at pit Shot Rock Spalls	24 – 48 hours 24 – 48 hours	
Tyrendarra Lime Pty Ltd Peter Milne Earthmoving Pty Ltd	40mm Limestone crushed 50mm Ballast 20mm Crushed Rock (Class 2, 3 & 4) 20mm Crushed Rock (NDCR) 40mm Crushed Rock (NDCR) 40mm Crushed Rock (Class 3)	2 days	

	400mm Crushed Rock (class 3	2 days
	Brown)	2 days
	19mm Crusher Run	2 days
	40mm Crusher Run	2 days
	20 / 40mm Drainage	2 days
	20 / 60mm Drainage	2 days
	Gravel loose at pit	2 days
	100 / 200mm Metal (Blue)	2 days
	100 / 200mm Metal (Brown)	2 days
	Shot Rock	•
		2 days
	Spalls	
	Top Soil	4.1.
Aussie Rock Pty Ltd	50mm Ballast	1 day
	20mm Crushed Rock (NDCR)	1 day
	40mm Crushed Rock (NDCR)	1 day
	14mm Crusher Run	1 day
	20 / 40mm Drainage	1 day
	40 / 60mm Drainage	1 day
	Sand (fine)	1 day
Moree Quarries	50mm Ballast	2 days
	20mm Crushed Rock (Class 1, 2	2 days
	& 3)	2 days
	20mm Crushed Rock (NDCR)	2 days
	5mm Blue Dust	2 days
	Shot Rock	2 days
	Spalls	2 days
	14mm Sealing Aggregate (Class	2 days
	A, B)	2 days
	14mm Sealing Aggregate (Pre-	2 days
	Coat)	2 days
	10mm Sealing Aggregate (Class A, B)	2 days
	10mm Sealing Aggregate (Pre-	
	Coat)	
	10mm Sealing Aggregate (Class	
	A, B)	
	10mm Sealing Aggregate (Pre-	
	Coat)	
WA Molan & Sons	20mm Crushed Rock (Class 2 &	1 day
30113	3)	1 day
	40mm Crushed Rock (Class 3)	1 day
	20 / 40mm Drainage	1 day
	Sand (Coarse)	1 day
	Spalls	,
Western Quarries Pty Ltd	50mm Ballast	
vvestern Quarries Pty Ltd	20mm Crushed Rock (Class 2, 3	
	, , ,	
	& 4)	
	20mm Crushed Rock (NDCR)	

	40mm Crushed Rock (NDCR)	
	40mm Crushed Rock (Class 3)	
	5mm Blue Dust	
	20 / 40mm Drainage	
	20 / 60mm Drainage	
	100 / 200 Metal (Blue)	
	Shot Rock	
	Spalls	
	Top Soil	
	14mm Sealing Aggregate (Class	
	A)	
	14mm Sealing Aggregate (Pre-	
	Coat)	
	10mm Sealing Aggregate (Class	
	A)	
	10mm Sealing Aggregate (Pre-	
	Coat)	
	10mm Sealing Aggregate (Class	
	A)	
	10mm Sealing Aggregate (Pre-	
	Coat)	
Mibus Bros (Aust) Pty Ltd	20mm Crushed Rock (Class 2, 3	4 weeks
	& 4)	2 days
	20mm Crushed Rock (NDCR)	2 days
	40mm Crushed Rock (NDCR)	1 week
	40mm Crushed Rock (Class 3	2 days
	and 4)	2 days
	19mm Crusher Run	2 days
	40mm Crusher Run	2 days
	5mm Blue Dust	2 days
	20mm Limestone Crushed	1 week
	40mm Limestone Crushed	1 week
	100 / 200 Metal (Blue)	2 days
	100 / 200 Metal (Brown)	2 days
	Shot Rock	
	Spalls	

#### Approximate required materials required per year;

50mm Ballast – 100tn

20mm Crushed Rock

- Class 1 50tn
- Class 2 10,000
- Class 3 100tn
- Class 4 100tn

20mm Crushed Rock (NDCR) – 100tn 40mm Crushed Rock (NDCR) – 10,000tn 40mm Crushed Rock (Class 3) – 100tn Crushed Rock (Brown) Class 4 – 100tn

19mm Crusher Run – 100tn

40mm Crusher run - 100tn

5mm Blue Dust - 500tn

20 / 40mm Drainage – 100tn

20 / 60mm Drainage - 100tn

Gravel loose at the pit – 7,500tn

20mm Limestone Crushed - 2,500tn

40mm Limestone Crushed – 2,500tn

100 / 200 Metal (Blue) – 50tn

100 / 200 Metal (Brown) - 50tn

Sand (Fine) – 1000tn

Sand (Course) - 500tn

7mm Scoria – 100tn

10mm Scoria – 100tn

14mm Scoria - 200tn

50mm Scoria 100tn

19 / 40mm Scoria Lime - 100tn

Shot Rock - 100tn

Spalls - 500tn

Top Soil – 750tn

14mm Sealing Aggregate (Class A & B) - 5000tn

14mm Sealing Aggregate (Pre-Coat) – 50tn

10mm Sealing Aggregate (Class A & B) – 4000tn

10mm Sealing Aggregate (Pre-Coat) – 50tn

10mm Sealing Aggregate (Class A &B) – 1000tn

10mm Sealing Aggregate (Pre-Coat) – 50tn

